### Direct Conversion in a Z-Pinch IFE Reactor

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### **Abstract**

Recently, a world's record x-ray power of 0.28 PW has been measured from a Z-pinch driven imploding plasma at Sandia National Laboratory, Albuquerque, NM. This result immediately led to detailed calculations showing high fusion energy gain from a Z-pinch indirectly driven DT fusion capsule. This has fueled interest in a practical Z-pinch fusion reactor. Formidable technological obstacles must be overcome to make a practical Z-pinch driven reactor. The pulsed power system must be capable of delivering 10<sup>7</sup> to 10<sup>8</sup> pulses of energy 20-50 MJ to the load with high efficiency (> 0.1) at a rate of ~ 0.3 pulses/s. The reactor chamber must be protected from fusion reactions and byproducts. The components destroyed must be cheap enough (~\$2/module).

An attractive scheme uses a MHD generator to directly convert most of the fusion energy with residual energy recovery by a steam bottoming cycle. A compact blanket absorbs most of the fusion energy and creates low temperature plasma that is used to drive a MHD generator. Rather low yields are required to convert the blanket to the  $\sim 1$  eV plasma required to optimally drive the MHD generator. For example, a 5 GJ yield requires a flibe blanket with a thickness of only  $\sim 20$  cm and a mass of  $\sim 70$  kg to absorb more that 1/2 of the fusion energy.

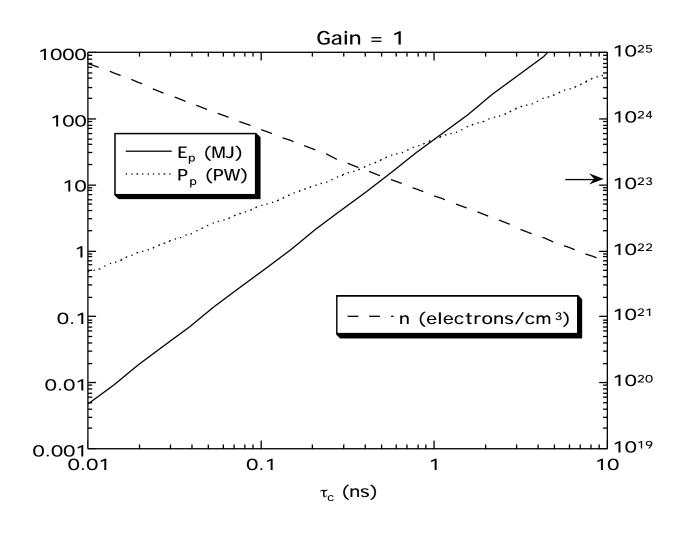
### Summary

- ☐ The key issues to be solved to produce a Z-pinch driven IFE reactor are:
  - **→** Accelerator requirements
    - → Rep rate ~ 0.1-1 pulse/sec.
    - $\rightarrow$  Energy to pinch > 20MJ.
  - **▶** Fusion Yield > 4 GJ.
    - $\rightarrow$  High gain is required (G > 150).
    - → Current Rise time as long as possible.
      - > Longer current rise time reduces the stress on accelerator design and allows higher load inductance.
  - Recyclable transmission line (RTL) and load must be cheap enough!
    - → Key requirement < \$2-3/pulse for RTL plus load.
  - **▶** Direct conversion is an attractive option

## The competition is tough!

- **□** Natural gas power plant (to be installed in Northern California)
  - **▶** Very low cost of electricity, COE ~ 3¢/kWh!
    - **→ HYLIFE, COE** ~9¢/kWh (1988)
  - **→** Low plant capital costs ~ 0.6\$/W!
    - → HYLIFE, ~ 3\$/W (1988)
  - **→** System efficiency ~ 60%
  - **→** We can not count on the greenhouse argument
    - → The carbon dioxide emission from natural gas plants has been reduced!
      - Carbon dioxide reduction increases the COE to 5¢/kWh
- **□** Wind generators are also in the running.
  - **→** COE ~ 5¢/kWh

## PW drivers are required IFE!



## Achievable accelerator output characteristics

- **□** Energy delivered to pinch  $\leq$  50 MJ.
- **☐** Wallplug Efficiency ~ 10-20%.
- $\square$  Rep. Rate = 0.1 1 pulse/sec.
- $\Box$  Long life ( ~ 10<sup>7</sup> pulses).

## **Z-pinch IFE reactor requirements**

- **☐** Accelerator requirements
  - **▶** Rep rate ~ 0.1 -1/sec.
  - $\rightarrow$  Energy to pinch > 20MJ.
- ☐ Fusion Yield > 1 GJ.
  - $\rightarrow$  High gain is required (G > 150).
  - **Current Rise time as long as possible.** 
    - → Longer current rise time reduces the stress on accelerator design and allows higher load inductance
- ☐ RTL and load must be cheap enough!
  - **▶** Key requirement ~ \$2/pulse for RTL and target.
  - **→** The present z-pinch experiments use wire arrays
    - → Wire arrays are probably to expensive to use in a reactor
    - → The wire arrays can be replaced by cheaper liners or gas puffs in the higher current reactor.

## The fusion gain must be high enough!

### **☐** The fusion gain must satisfy:

$$\eta_E G_{fusion} \eta_{x-ray} \eta_A f = 1$$

$$\eta_{x-ray} = 0.8$$

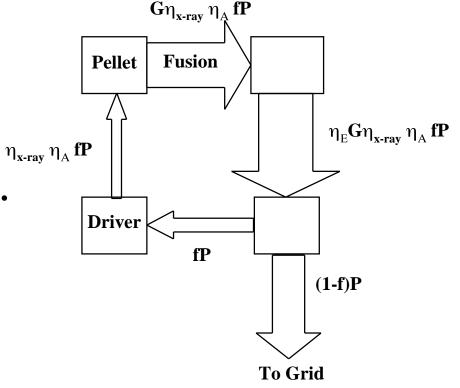
 $\eta_E$  = 0.4, Electrical energy/thermal energy.

 $\eta_A = 0.1$ , Accelerator efficiency, pinch energy/accelerator energy.

f = 0.2, Recirculating power fraction.

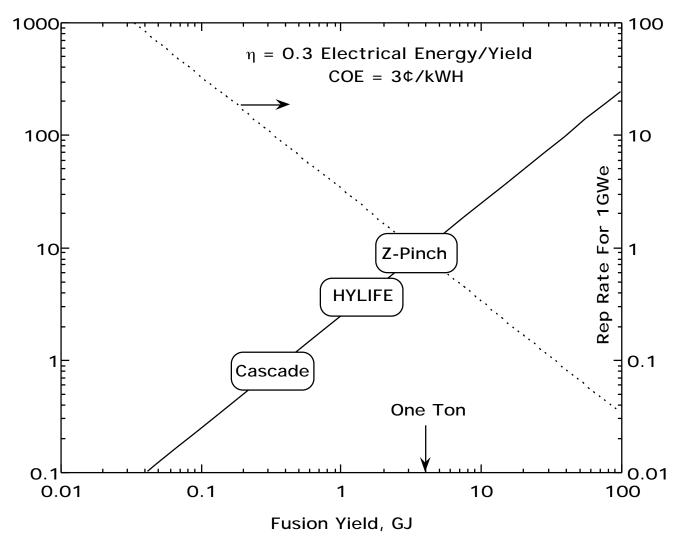
$$G_{\text{fusion}} > 150$$

 $\Box$  High gain (G > 150) is required.



## High yield increases the allowed sacrificial component cost

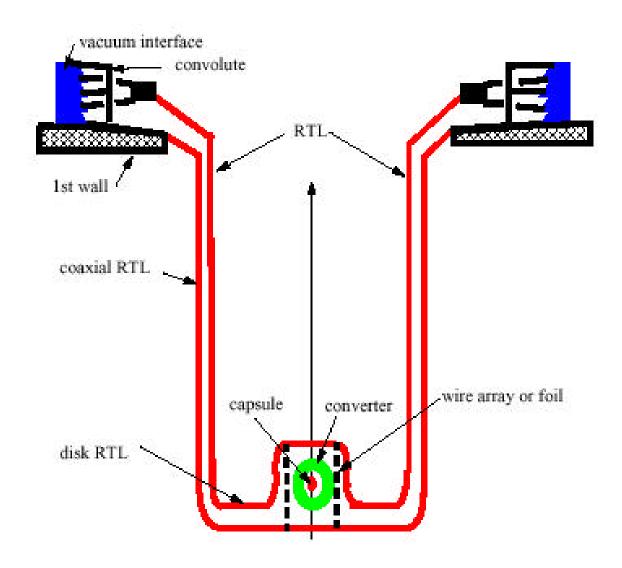
- < \$2/pulse for sacrificial components (SC/V~ 5)
- Low yield schemes (\$\frac{1}{2} 0.1) require high rep rates, > 30 pulses/sec and low Schemes cost < 5¢/pulse



## High gain Z-pinch driven IFE capsules have been designed

- **Z-pinch driven hohlraum design** (J. H. Hammer, M. Tabak, S. C. Wilks, J. D. Lindl, D. S. Bailey, P. W. Rambo, A. Toor, and G. B. Zimmerman, "High Yield Inertial Confinement Fusion Target Design for a Z-pinch Driven Hohlraum," Phys. Plasmas **6**, 2129 (1999)) has a gain of **75**.
  - **→** Accelerator requirements
    - → 100 ns current risetime
    - → 60MA peak current
  - → ~ 16MJ of x-rays from pinch required
  - **▶** 1.2 GJ Yield
  - **→** Higher gain is required

## Schematic of recyclable transmission line



# Direct energy MHD conversion is an attractive option

#### ☐ The scheme:

- Deposit the fusion energy in a compact blanket.
- → Vaporize/ionize the blanket to produce a highly conductive plasma (T ~ 1 eV).
- **→** The plasma is expanded through a nozzle and a MHD generator to directly produce electricity.

#### References

- 1. E. P. Velikov, V. S. Golubev, V. V. Chernukha, Soviet Atomic Energy <u>36</u>, 258 (1974).
- 2. G. P. Lasche, Unpublished UCD Ph. D. dissertation, UCRL 53434, LLNL (1983).

# Compact Fusion Advanced Rankine MHD Conversion (Grant Logan)

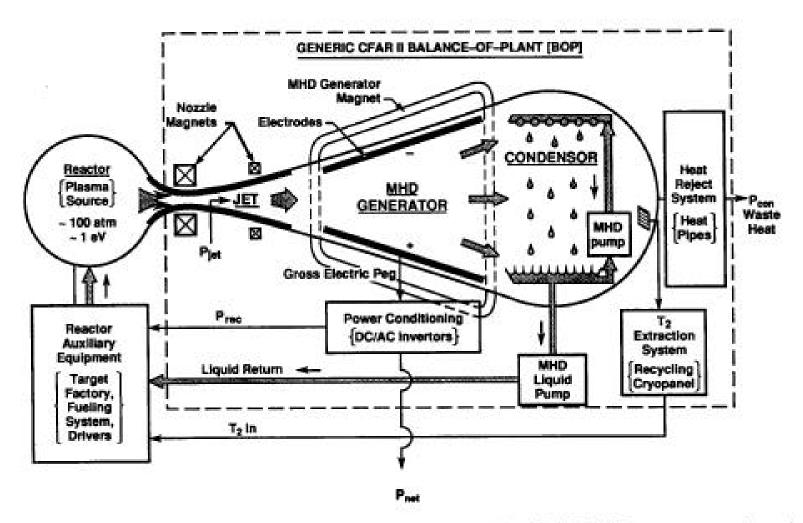


Figure 1 General scheme for Compact Fusion Advanced Rankine (CFARII) MHD-power-conversion cycle

# The optimum Flibe blanket outer radius varies slowly with yield

☐ The optimum Flibe (fluorine, lithium, and berylium) blanket thickness varies slowly with yield.

	Blanket Outer		Energy Capture	
	Radius			
Yield	$\mathbf{r}_{ ext{outer}}$	Mass	Fc	COE
5GJ	<b>18cm</b>	<b>50kg</b>	.55	38 (mills/kWe)
10	20	<b>68kg</b>	.60	33
20	25	132kg	.75	30

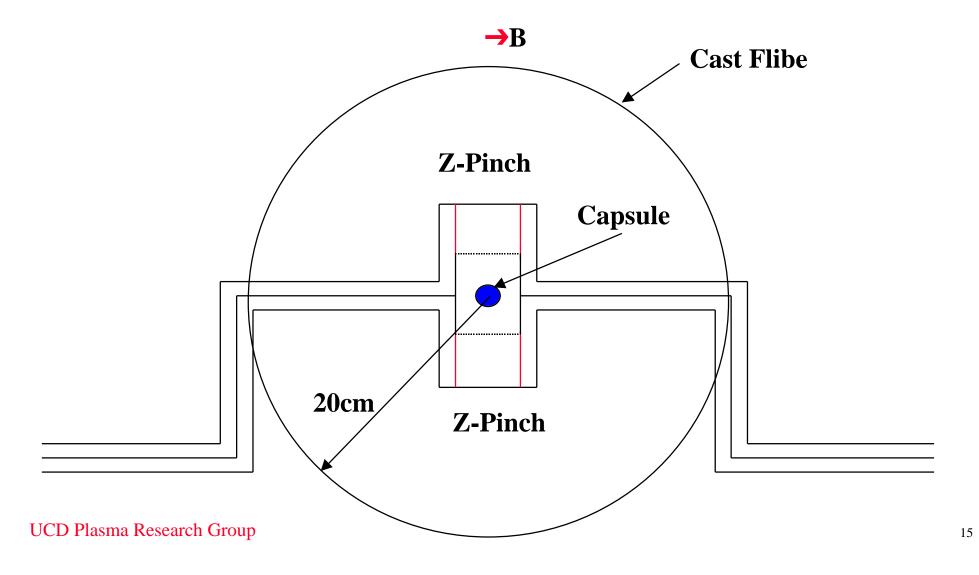
 $P_{fusion}$  = 4GW, Fusion Target Gain = 1000, Driver cost = 4\$/J Driver efficiency = 0.2

From: B. G. Logan, <u>Low cost</u>, <u>High Yield IFE Reactors: Revisiting Velikhov's Vaporizing Blankets</u>, Fusion Technology, 21, 1784 (1992).

See also: B. G. Logan, <u>Inertial fusion reactors using Compact Fusion</u>
<u>Advanced Rankine (CFARII) MHD conversion</u>, Fusion Engineering and Design <u>22</u>, 151 (1993).

# Most of the fusion energy is deposited in the compact blanket

### Compact blanket



### UC Davis z-pinch IFE research program

- ☐ The Plasma Research Group will evaluate the impact of the RTL on power plant design
  - **▶** The RTL is connected to the target to drive the imploding z-pinch load.
    - → The connection of the RTL to the permanent MITL must survive.
    - → The RTL close to the target (fusion capsule + hohlraum) will be transformed into hot plasma and shrapnel.
    - → The power plant must be designed so that the reactor components are protected from the shrapnel.
  - **→** We will calculate
    - → Neutron and x-ray emission from the high temperature plasma.
    - → Molecular dynamics calculations of the size distribution of the shrapnel.
    - → The effect of the shrapnel on the reactor components.
- $lue{}$  We will also evaluate the viability of direct conversion.